

Problem 2.1. Equalizer Design. 21 points.

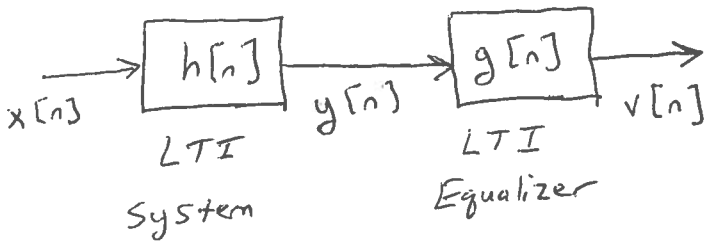
This problem asks you to design an equalizer to compensate for the magnitude and phase distortion of a discrete-time linear time-invariant (LTI) system.

(a) Describe how you would estimate the impulse response of the discrete-time LTI system. 6 points.

A discrete-time LTI system is uniquely characterized by its impulse response, $h[n]$.

For an unknown $h[n]$, input a maximal-length pseudo-noise sequence $x[n]$ and observe $y[n]$: and either backsolve for $h[n]$ in $y[n] = x[n] * h[n]$ or compute $H(\omega) = \frac{Y(\omega)}{X(\omega)}$ and take the inverse discrete-time Fourier transform.

(b) For a discrete-time LTI system with impulse response $h[n] = \delta[n] - a\delta[n-1]$ where a is a real number, design a stable discrete-time LTI equalizer so that the impulse response of the cascade of the discretized channel and equalizer yields a delayed impulse. Your approach must handle all possible values of a . 15 points.



A maximal-length pseudo-noise sequence has all frequencies in it, and hence $X(\omega)$ never equals zero.

We want the cascade of $h[n]$ and $g[n]$ to be an all-pass

LTI system: $h[n] * g[n] = C_0 \delta[n - n_0]$
constant gain constant delay

$$H(z) G(z) = C_0 z^{-n_0}$$

$$G(z) = C_0 \frac{z^{-n_0}}{H(z)} ; H(z) = 1 - a z^{-1}$$

Case I: $|a| < 1$. Use pole-zero cancellation for cascade of $H(z)$ and $G(z)$:

$$G(z) = \frac{C_0 z^{-n_0}}{1 - a z^{-1}}$$

Case II: $|a| = 1$. Zero of $H(z)$ is on the unit circle; hence, the frequency of the zero is eliminated and cannot be recovered. Use notch configuration:

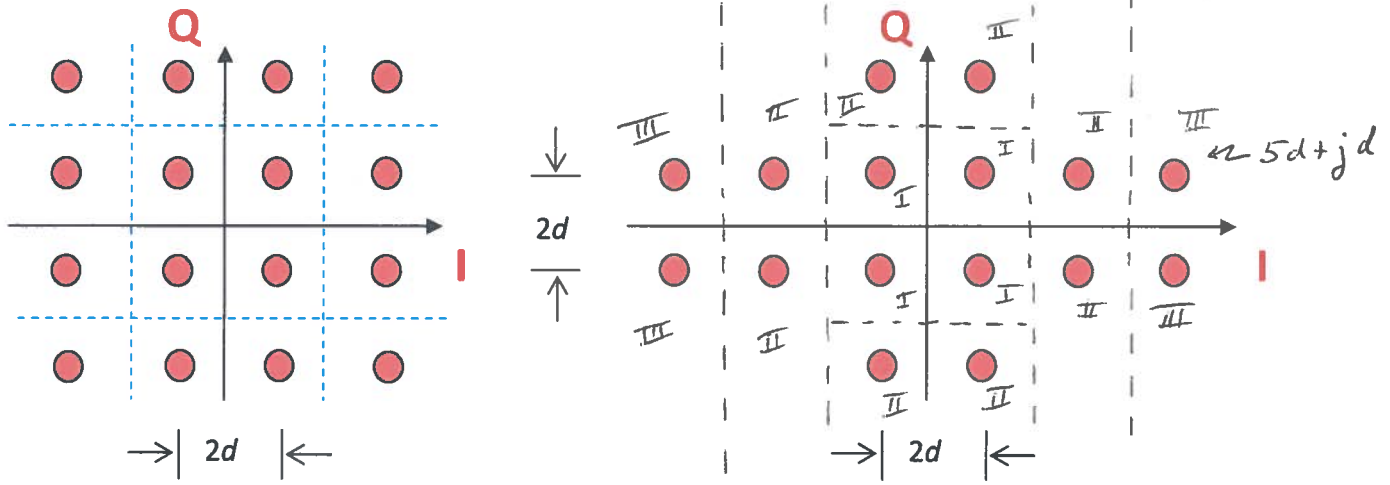
$$G(z) = \frac{C_0 z^{-n_0}}{1 - 0.95 \operatorname{sgn}(a) z^{-1}}$$

Case III: $|a| > 1$. Use all-pass configuration for cascade of $H(z)$ and $G(z)$:

$$G(z) = \frac{C_0 z^{-n_0}}{1 - \frac{1}{a} z^{-1}}$$

Problem 2.2 QAM Communication Performance. 27 points.

Consider the two 16-QAM constellations below. Constellation spacing is $2d$.



Energy in the pulse shape is 1. Symbol time T_{sym} is 1s. The constellation on the left includes the decision regions with boundaries shown by the in-phase (I) axis, quadrature (Q) axis and dashed lines.

	Left Constellation	Right Constellation
(a) Peak transmit power	$18d^2$	$26d^2$
(b) Average transmit power	$10d^2$	$12d^2$
(c) Number of type I regions	4	4
(d) Number of type II regions	8	8
(e) Number of type III regions	4	4
(f) Probability of symbol error for additive Gaussian noise with zero mean & variance σ^2	$3Q\left(\frac{d}{\sigma}\right) - \frac{9}{4}Q^2\left(\frac{d}{\sigma}\right)$	$3Q\left(\frac{d}{\sigma}\right) - \frac{9}{4}Q^2\left(\frac{d}{\sigma}\right)$

Draw the decision regions for the right constellation on top of the right constellation. 3 points.

I and Q axes are also decision boundaries.

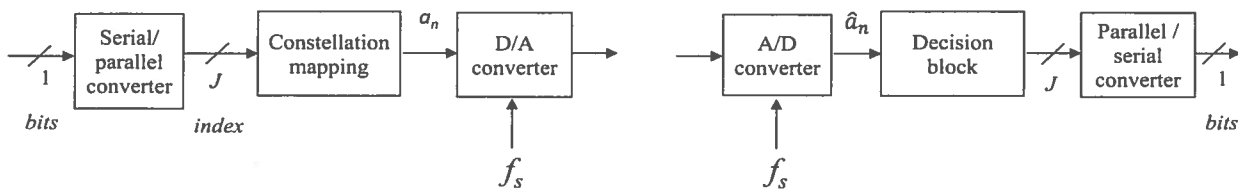
Fill in each entry (a)-(f) in the above table for the right constellation. Each entry is worth 3 points.

Which of the two constellations would you advocate using? Why? 6 points.

The left constellation is the better choice because it has

1. Lower peak transmit power
2. Lower average transmit power
3. Lower peak-to-average power ratio
4. Lower probability of symbol error vs. SNR
5. Gray coding whereas the right one does not.

Problem 2.3. Automatic Gain Control. 30 points. Using decision-directed feedback.
 Consider the simplified transmitter (left) and receiver (right) for baseband pulse amplitude modulation:



System uses J bits per symbol and a constellation spacing of $2d$ in units of Volts.

Your goal is to design an automatic gain control system for the receiver to compensate for fading:

- Fading is modeled as an unknown time-varying gain $g(t)$ or $g[n]$.
- The decision block will feed back the following signal to the automatic gain control system

$$v[n] = \hat{a}_n - a_n$$
 where \hat{a}_n is the received symbol amplitude and a_n is the transmitted symbol amplitude.
- The automatic gain control system will adapt its gain $c[n]$ so that estimated symbol amplitudes will become closer in value to the transmitter symbol amplitudes over time.

(a) Determine an objective function $J(v[n])$. 6 points.

$$J(v[n]) = \frac{1}{2} v^2[n]$$

$$v[n] = \hat{a}_n - a_n$$

$$\hat{a}_n = g[n] c[n] a_n$$

$$v[n] = (g[n] c[n] - 1) a_n$$

(b) Based on your objective function in (a), derive an update equation to adapt $c[n]$. 9 points.

$$c[n+1] = c[n] - \bar{\mu} \frac{dJ(v[n])}{dc[n]}$$

$$c[n+1] = c[n] - \mu v[n] a_n$$

$$\frac{dJ(v[n])}{dc[n]} = g[n] a_n v[n]$$

where $\mu = g[n] \bar{\mu}$ but μ is treated as a constant. ~~unknown~~

(c) For the answer in (b), what value of the step size would you recommend? Why? 3 points.

We want $0 < \bar{\mu} < 1$. In practice, keep $\bar{\mu}$ small, e.g. 0.001.

Then, μ is the minimum value of $|g[n]|$ times $\bar{\mu}$.

(d) Propose an algorithm to find an initial accurate value of $c[n]$. 6 points

- Use a training sequence so that a_n is known to the receiver and apply the above algorithm, or
- Use the automatic gain control method from QAM receiver lecture:

$$c[n] = (1 + 2f_0 - f_{\max} - f_{\min}) c[n-1]$$
 where f_0 is frequency of $a_n = 0$,

(e) Modify your update equation for $c[n]$ in (b) to improve convergence for $c[n]$ when $g[n]$ is varying quickly with time. 6 points.

- Use a smaller step size, or
- Replace $v[n]$ with an average of the current $v[n]$ and its previous M values (via a lowpass filtering of $v[n]$).

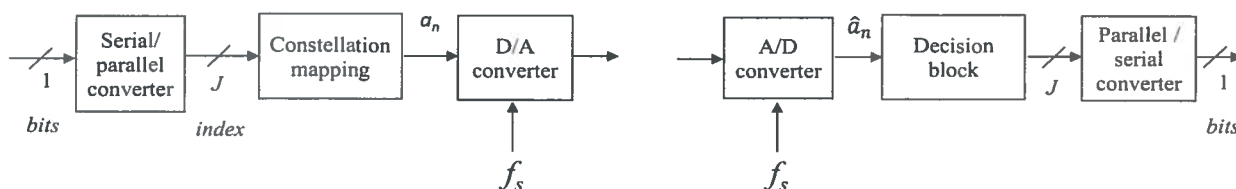
and f_{\max} is frequency of $a_n = 2^{J-1} - 1$,
 and f_{\min} is frequency of $a_n = -2^{J-1}$.

Initial values: $f_0 = f_{\min} = f_{\max} = \frac{1}{2^J}$

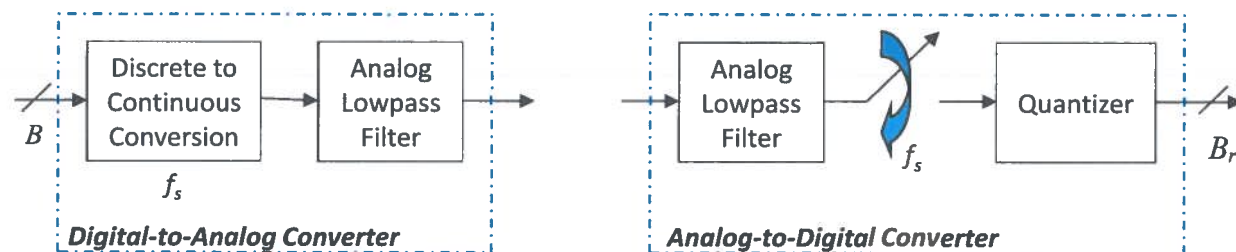
Note that $N_g = 1$ symbols/pulse
and $L = 1$ sample/symbol.

Problem 2.4. Data Converter Design. 22 points

Consider the simplified transmitter (left) and receiver (right) for baseband pulse amplitude modulation



Here are block diagrams for the analog-to-digital (A/D) and the digital-to-analog (D/A) converters:



Communication system uses J bits per symbol and a constellation spacing of $2d$ in units of Volts.

The channel model consists of additive spectrally-flat Gaussian noise with zero mean and variance σ^2 .

(a) In the transmitter, what is the smallest number of bits B needed for the D/A Converter? 6 points.

$B = J$

Note: In this case, each constellation point is separated by one quantization level, and $2d$ is the step size: $\frac{V_{max} - V_{min}}{Levels - 1}$ where $Levels = 2^J$.

(b) In the transmitter, what is the second smallest number of bits that could be used for the D/A Converter? 6 points.

$B = J + 1$

Note: In this case, each constellation point is separated by two quantization levels.

(c) In the receiver, what is the minimum number of bits B_r needed for the A/D Converter so that the quantization noise power at the quantizer output in the A/D Converter is less than or equal to the system noise power at the quantizer input? 10 points.

$\sigma^2 \geq \sigma_Q^2$ where $\sigma_Q^2 = \frac{1}{3} V_{max}^2 2^{-2B_r}$ on slide 8-13.

System noise power Quantization noise power

$$\sigma^2 \geq \frac{1}{3} V_{max}^2 2^{-2B_r} \Rightarrow \frac{3\sigma^2}{V_{max}^2} \geq 2^{-2B_r} \Rightarrow \log_2 \frac{3\sigma^2}{V_{max}^2} \geq -2B_r$$

non-negative non-negative

$$B_r \geq \left\lceil \log_2(V_{max}) - \log_2(\sqrt{3}\sigma) \right\rceil$$

ceiling operation