Multidimensional Sampling

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Motivation for the General Case for Sampling

We need the more general case to treat three important applications.

- 1. Human Vision System: the human vision system is a nonlinear, spatiallyvarying, non-uniformly sampled system. Rods and cones on the retina, which spatially sample are not arranged in rows and columns.
- a. Hexagonal Sampling: when modeled as a linear shift-invariant system, the human visual system is circularly bandlimited (lowpass in radial frequency). The optimal uniform sampling grid is hexagonal. Optimal means that we need the fewest discrete-time samples to sample the continuous-space analog signal without aliasing.
- b. Foveated grid: This is based on the fovea in the retina. When you focus on an object, you sample the object at a high resolution, and the resolution falls off away from the point-of-focus. Shown below is a simple example of a foveated grid. The grid is a 4 x 4 uniform sampling with each of the middle four grids subdivided into 4 x 4 grids themselves. The point of focus is at the middle of the grid. We can convert this grid to a uniform grid in several ways. For example, we could start with a rectangular grid and keep the resolution at the point-of-focus. Then, away from the point-of-focus, we can average the pixel values in increasingly larger blocks of samples. This approach allows the use a foveated grid while maintaining compatibility with systems that require rectangular sampling (e.g. image and video compression standards).



2. Television



650 samples /row 362.5 rows /interlace 2 interlaces /frame 30 frames /sec

No two samples taken at the same instant of time

Can signals be sampled this way without losing information?

How can we handle

- a. standard conversion
- b. interlace removal
- c. motion compensation

Periodic Sampling Lattices



An *M*-dimensional periodic sampling lattice (grid) can be formed by taking integer combinations of a set of *M* linearly independent vectors.

$$\begin{split} t_1 &= v_{11}n_1 + v_{12}n_2 \\ t_2 &= v_{21}n_1 + v_{22}n_2 \qquad \iff \quad \vec{t} = \mathbf{V}\vec{n} \quad (in\ 1 - D\ t = Tn\) \end{split}$$

where \mathbf{V} is the sampling matrix (2 x 2 in this case)

$$x(\vec{n}) = x_a(\mathbf{V}\vec{n})$$

In the rectangular case,

$$\mathbf{V} = \begin{bmatrix} T_1 & 0 \\ 0 & T_2 \end{bmatrix}$$

Continuous Fourier Transform

$$X_{a}(\vec{\Omega}) = \int_{-\infty}^{+\infty} x_{a}(t) e^{-j\vec{\Omega}^{T}t} dt$$
$$x_{a}(t) = \frac{1}{(2\pi)^{M}} \int_{-\infty}^{+\infty} X_{a}(\vec{\Omega}) e^{j\vec{\Omega}^{T}t} d\vec{\Omega}$$

Relevant Properties

$$\dot{x_a(t)} * \dot{h_a(t)} \leftrightarrow X_a(\vec{\Omega}) H_a(\vec{\Omega})$$

$$\dot{x_a(t)} p_a(t) \leftrightarrow \frac{1}{(2\pi)^M} X_a(\vec{\Omega}) * P_a(\vec{\Omega})$$

Derivation

 $p_a(\bar{t})$ is a field of impulses (bed of nails) as before:

$$p_{a}(\vec{t}) = \sum_{\vec{n}} \delta(\vec{t} - \vec{\mathbf{V}n})$$
$$P_{a}(\vec{\Omega}) = \frac{(2\pi)^{M}}{|\det \mathbf{V}|} \sum_{\vec{k}} \delta(\vec{\Omega} - \vec{\mathbf{U}k})$$

where **U** is defined by $\mathbf{V}^{\mathrm{T}}\mathbf{U} = 2 \pi \mathbf{I}$ such that **I** is the identity matrix and **U** is the periodicity matrix.

Example: For the rectangular case,

$$\mathbf{U} = \begin{bmatrix} \frac{2\pi}{T_1} & 0\\ 0 & \frac{2\pi}{T_2} \end{bmatrix}$$

Sample the analog continuous-space signal

$$\widetilde{x}_{a}(t) = x_{a}(t)p_{a}(t)$$

Under integration, the sampled representation simplifies to

$$\tilde{x}_{a}(t) = \sum_{\vec{n}} \vec{x(n)} \delta(t - \vec{\mathbf{V}n})$$

Taking its Fourier transform

$$\widetilde{X}_{a}(\overrightarrow{\Omega}) = F\left\{x_{a}(\overrightarrow{t})p_{a}(\overrightarrow{t})\right\} = \frac{1}{\left|\det \mathbf{V}\right|} \sum_{\vec{k}} X_{a}(\overrightarrow{\Omega} - \mathbf{U}\overrightarrow{k})$$

The aliased analog spectrum, where $x(\vec{n}) = x_a(\mathbf{V}\vec{n})$, is

$$X(\vec{\omega}) = \sum x(\vec{n})e^{-j\omega^{T}\vec{n}} = \frac{1}{|\det \mathbf{V}|} \sum_{\vec{k}} X_{a} \left(\mathbf{V}^{-T}(\vec{\omega} - 2\pi\vec{k}) \right)$$

The Discrete-Time Fourier Transform of the sampled signal is

$$X(\vec{\Omega}) = \sum_{\vec{n}} x(\vec{n}) e^{-j\vec{\Omega}^T \mathbf{V}\vec{n}} = \frac{1}{\left|\det \mathbf{V}\right|} \sum_{\vec{k}} X_a(\vec{\Omega} - \mathbf{U}\vec{k})$$

so $\vec{\omega} = \mathbf{V}^T \vec{\Omega}$ (in 1-D case: $\boldsymbol{\omega} = T \boldsymbol{\Omega}$). The term $|\det \mathbf{V}|$ is the spatial domain area associated with each sample:

$$\frac{1}{|\det \mathbf{V}|} = sampling \ density = \frac{|\det \mathbf{U}|}{(2\pi)^M} samples / area$$

The factor of $(2\pi)^M$ is due to the det $\alpha \mathbf{A} = \alpha^M \det \mathbf{A}$ for scalar α . If we have control over the sampling lattice, we find **V** by choosing **U** such that 1. there is no aliasing (depends on the bandwidth of $x_a(t)$)

2. $|\det U|$ is as small as possible

Then $\mathbf{V} = 2\pi \mathbf{U}^{-T}$. **U** is called the aliasing or polar matrix.

A lattice is the set of points generated by a sampling matrix according to $\{V\vec{n} : \vec{n} \in \vec{I}\}$. V has real-valued elements. In the context of the discrete-space domain, V has integer-valued elements. V must be non-singular.

Example: In the 2-D frequency domain, consider



How tightly can we "tile the plane" without aliasing?

$$\vec{u}_{1} = \begin{bmatrix} W \\ W \end{bmatrix}; \quad \vec{u}_{2} = \begin{bmatrix} W \\ -W \end{bmatrix}; \quad \mathbf{U} = \begin{bmatrix} W & W \\ W & -W \end{bmatrix}; \quad \mathbf{V} = \begin{bmatrix} \pi/W & \pi/W \\ \pi/W & -\pi/W \end{bmatrix}$$
$$\frac{|\det \mathbf{U}|}{4\pi^{2}} = \frac{W^{2}}{2\pi^{2}} = \frac{1}{|\det V|} (in \ samples \ / \ area)$$

Special Case: 1-D

$$\begin{aligned} x(n) &= x_{a}(Tn) \\ \mathbf{V} &= T \ (scalar) \\ \mathbf{U} &= \frac{2\pi}{T} \ (scalar) \\ X(\omega) &= \frac{1}{|\det \mathbf{V}|} \sum_{\vec{k}} X_{a} (\mathbf{V}^{-T} (\vec{\omega} - 2\pi \vec{k})) = \frac{1}{T} \sum_{k} X_{a} (\frac{\omega}{T} - \frac{2\pi k}{T}) \\ \text{sampling density} &= \frac{1}{T} \ (\text{samples/sec}) \\ \text{preventing aliasing} : 2\mathbf{W} &< \frac{2\pi}{T} \quad (\mathbf{W} < \frac{\pi}{T}) \end{aligned}$$