### **Optimal Design of Real and Complex Minimum Phase Digital FIR Filters**



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# **Minimum Phase Digital FIR Filters**

#### • Properties

- All zeros are on or inside the unit circle in the *z*-plane
- Twice as many free parameters as linear phase filters of the same length
- Minimum group delay
- Minimum length to meet piecewise constant magnitude specifications

#### Impulse Responses





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# **Minimum Phase FIR Filter Design Algorithms**

- Spectral Factorization [Chen & Parks 1986]
  - 1. Design linear phase filter for minimum phase power spectrum
  - 2. Factor polynomial transfer function
  - **3. Reconstruct minimum phase polynomial transfer function**
- Cepstral Deconvolution [Boite & Leach 1981][Mian & Nainer 1982]
  - **1.** Compute amplitude function for desired magnitude response
  - 2. Calculate *unique* minimum phase function using complex cepstrum
  - **3.** Apply inverse fast Fourier transform (FFT) or solve nonlinear equations

| Characteristic             | Spectral<br>Factorization | Cepstral<br>Deconvolution | Proposed<br>Algorithm |
|----------------------------|---------------------------|---------------------------|-----------------------|
| Computation                | Iterative                 | Non-Iterative             | Non-Iterative         |
| Coefficient Accuracy       | High                      | Low                       | User Controlled       |
| Coefficient Data Type      | Real                      | Real                      | Real or Complex       |
| Magnitude<br>Specification | Piecewise<br>Constant     | Arbitrary                 | Arbitrary             |
| Dimensions                 | 1-D only                  | 1-D                       | 1-D or <b>m-D</b>     |

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# **Proposed Algorithm**

#### **1. Determine desired amplitude response** $|X(e^{j\omega})|$

- *Choice #1*: Piecewise constant magnitude response
  - Convert minimum phase filter design specifications to optimal linear phase filter specifications
  - Design optimal linear phase filter
  - Transform amplitude response to match that of desired optimal minimum phase filter using formulas by Chen and Parks
- *Choice #2:* Specify an arbitrary magnitude response

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# **Proposed Algorithm**

2. Compute *unique* phase response from amplitude response

• Use generalized Discrete Hilbert Transform relation for a causal minimum phase sequences

$$\arg X(e^{j\omega}) = -\frac{1}{2\pi} \int_{-\pi}^{\pi} \log |X(e^{j\omega})| \cot\left(\frac{\omega-\theta}{2}\right) d\theta - K$$

- For real coefficients, *K* = 0 [Cizek 1970]
- For complex case, we show that *K* is a constant, which disappears when taking the derivative of the phase to calculate group delay

#### **3.** Compute the impulse response

- Sample magnitude and phase response at *M* points
- Compute inverse FFT and truncate the result

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### **Real Minimum Phase Bandpass Filter Design**



**Proposed algorithm** (near-linear phase passband): **50 taps Parks-McClellan algorithm** (linear phase): **99 taps** 

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### **Complex Minimum Phase Lowpass Filter Design**



**Proposed algorithm** (near-linear phase passband): 26 taps Karam-McClellan algorithm (linear phase passband): 51 taps

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### Conclusion

#### • Algorithm based on the Discrete Hilbert Transform (DHT)

- Extension of the DHT relations to complex sequences
- Optimal design algorithm for real and complex minimum phase FIR filters
- Error bounds for real and complex filters
- FFT length required to compute the DHT for a given coefficient accuracy

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# **Order of the FFT**

- Algorithm imposes causality on complex cepstral sequence
  - Complex cepstral sequence *x*(*n*) has infinite duration
  - Truncation of x(n) to M samples introduces error
  - User specifies coefficient accuracy as  $\boldsymbol{\epsilon}$
  - Constraint on maximum error becomes
  - Given  $\varepsilon$ , compute number of stopband zeros  $N_s$  and FFT length  $M = 2^m$

 $\left|x\left(\frac{M}{2}\right)\right| < \varepsilon$ 

• Complex filter case (loose upper bound is  $M = 2 N_s / \epsilon$ )

$$m = \left\lceil 1 + \log_2 N_s - \log_2 \varepsilon \right\rceil$$

- Tighter bound for real filter case (new result not in paper)
  - Stopband zeros are complex conjugate pairs spaced uniformly on unit circle

$$m = \left\lceil 2 + \log \left| \sum_{l=0}^{l} \cos\left(2\pi \left(f_s + i\frac{1-2f_s}{N_s-1}\right)\right) \right| - \log_2 \varepsilon \right\rceil$$
  
•  $f_s$  is the stopband frequency and  $l = \left\lfloor \frac{(N_s-1)}{2} \right\rfloor$   
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