

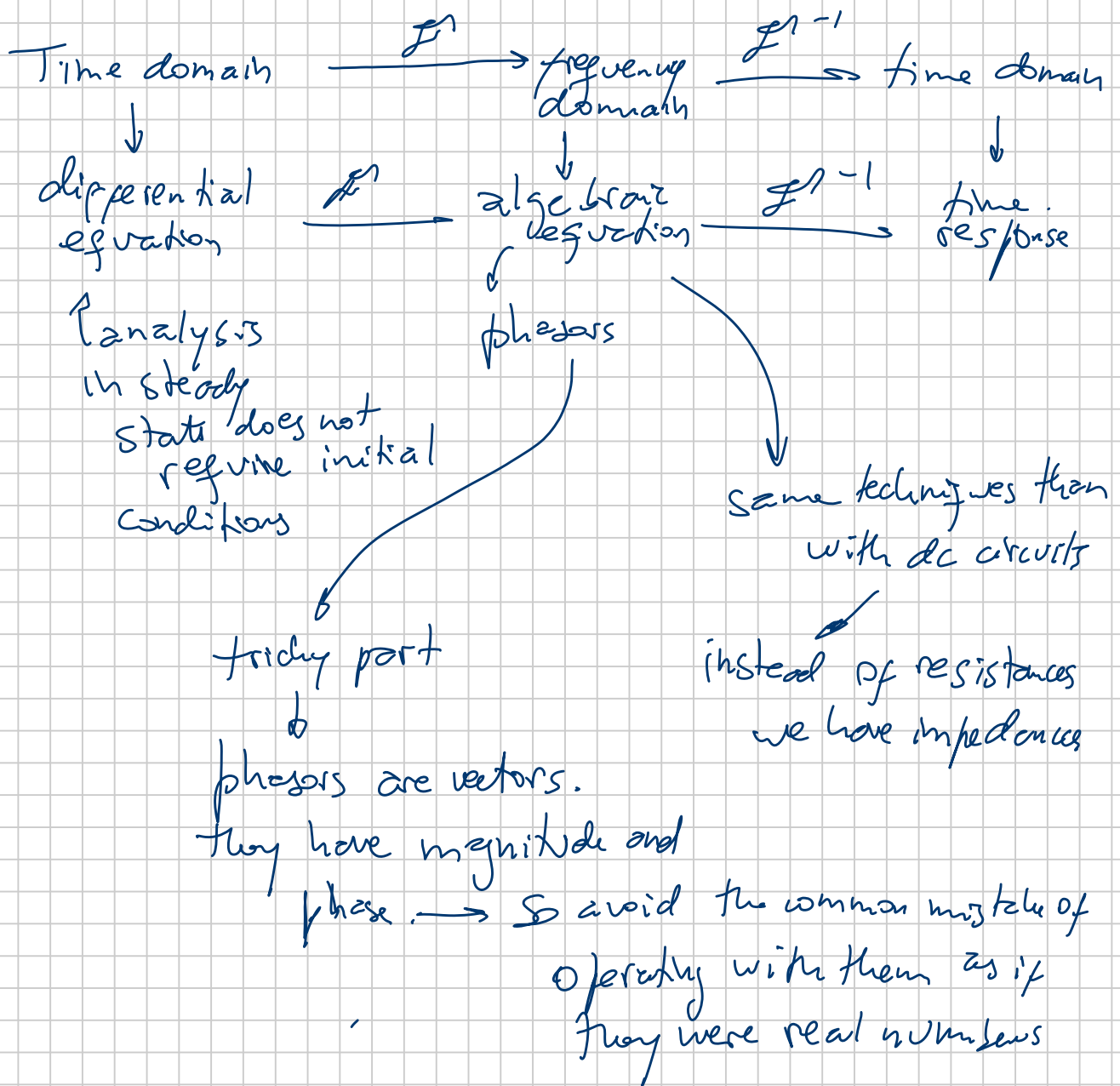
EE411 Sinusoidal steady state analysis

Note Title

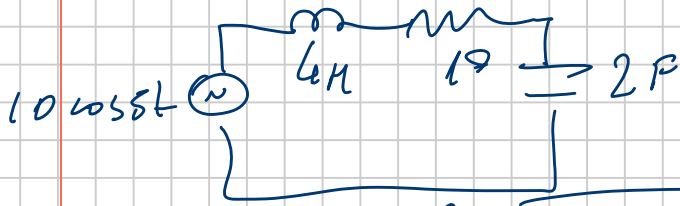
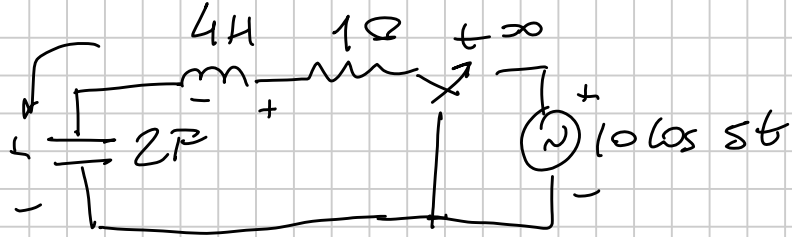
7/15/2008

Analysis is only for steady state, NOT for transient.

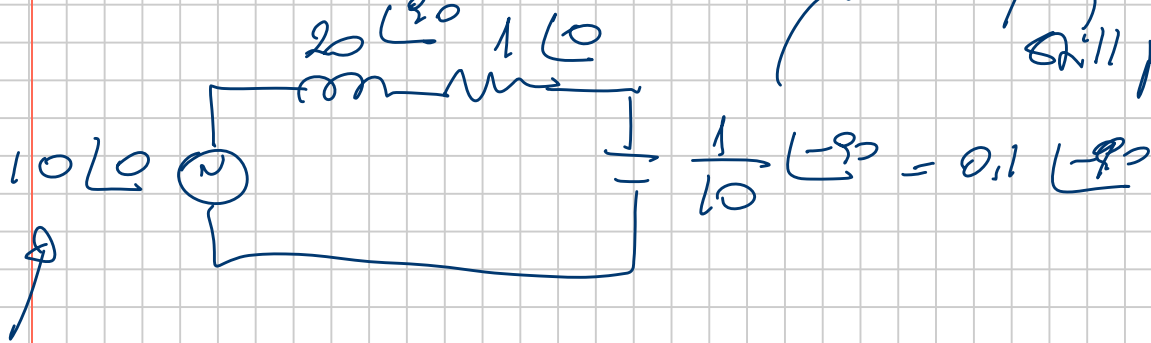
- Steps \rightarrow
- 1) Transform the circuit to the frequency domain
 - 2) Solve the problem using the techniques discussed with dc circuits (nodal analysis, etc)
 - 3) Transform back to the time domain.



Circuit used in 2nd order system analysis →



But frequency information still persists here



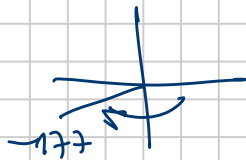
frequency information is lost here

$$\underline{I} \quad \underline{Z} = \underline{V}_s = 10 \angle 0$$

$$\underline{Z} = 20 \angle 90 + 1 \angle 0 + 0.1 \angle -90 = 19.92 \angle 87.12$$

$$\underline{I} = \frac{10 \angle 0}{19.92 \angle 87.12} = 0.5 \angle -87.12$$

$$\underline{V}_c = \underline{I} \underline{Z}_c = 0.1 \angle -90 \cdot 0.5 \angle -87.12 = 0.05 \angle -177.12$$



Steady state

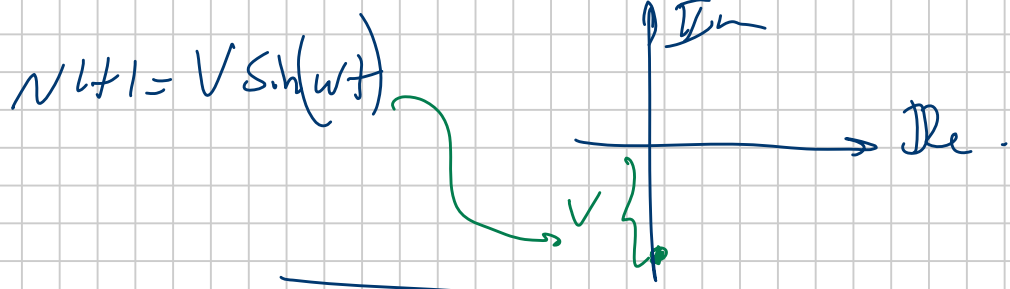
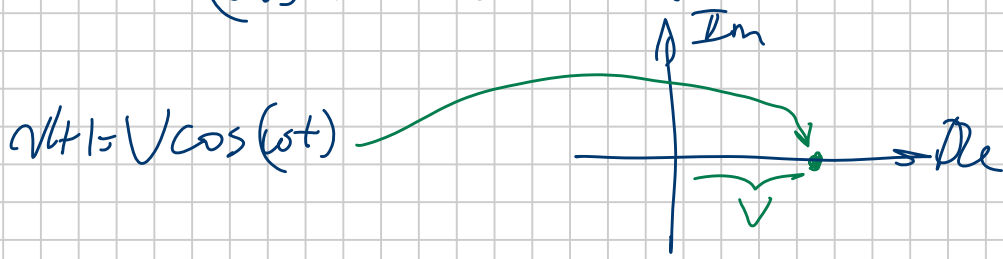
$$v_c(t) = 0.05 \cos(5t - 177.12) = A \cos(5t) + B \sin(5t)$$

$$A = 0.05 \cos(177.12) \approx -0.05$$

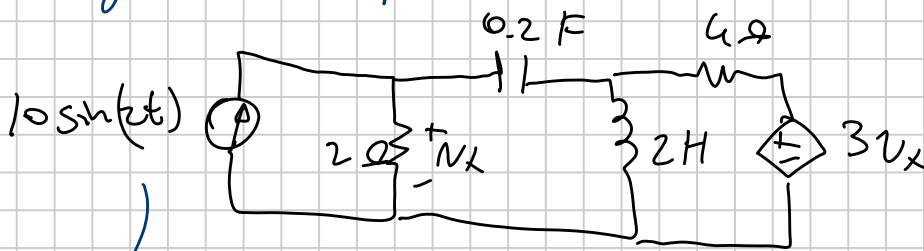
$$B = 0.05 \sin(177.12) \approx 0.0025$$

$$v_c(t) = -0.05 \cos(5t) + 0.0025 \sin(5t)$$

Note $V \sin(\omega t) = V \cos(\omega t - 90^\circ) \rightarrow \underline{V} = V \angle -90^\circ$



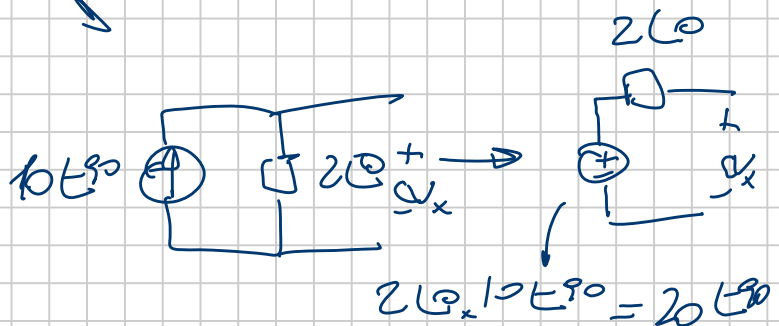
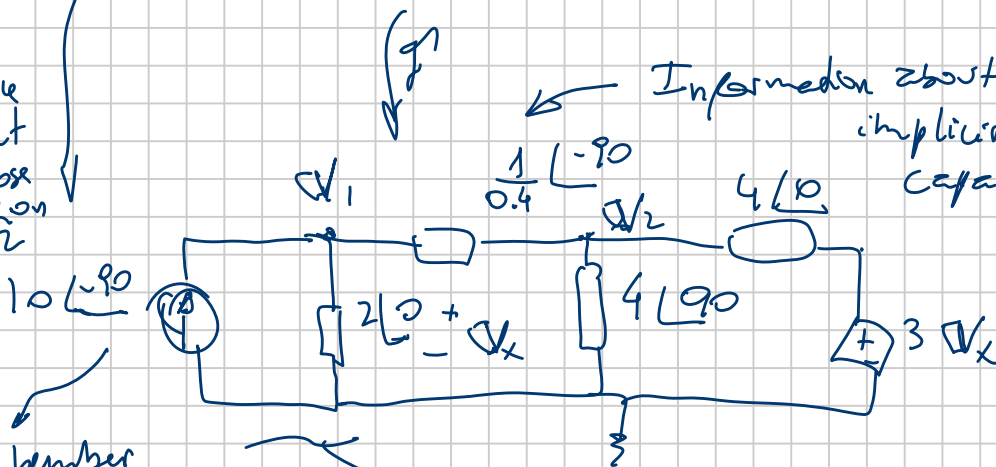
e.g. practice problem 10.1

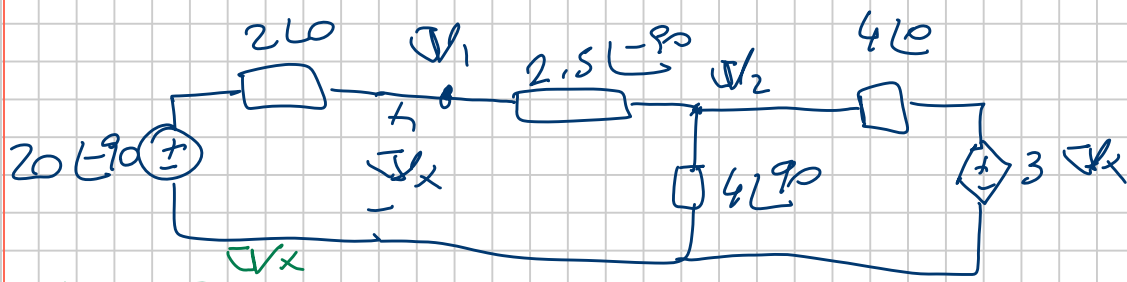


Note that we lose information about $\omega=2$

Remember that phase of phasors is with respect to cos function

Information about $\omega=2$ still survives implicitly within the capacitors and inductors impedances





#1

$$20\angle-90 - 2\angle0 I_{m1} - 2.5\angle-90 I_{m1} - 4\angle90 (I_{m1} - I_{m2}) = 0$$

$$2.5\angle36.89 I_{m1} - 4\angle90 I_{m2} = 20\angle-90$$

#2

$$-4\angle90 (I_{m2} - I_{m1}) - 4\angle0 I_{m2} - 60\angle-90 + 6\angle0 I_{m1} = 0$$

$$-7.21\angle33.7 I_{m1} + 5.65\angle45 I_{m2} = -60\angle-90$$

$$\begin{cases} 2.5\angle36.89 I_{m1} - 4\angle90 I_{m2} = 20\angle-90 \\ -7.21\angle33.7 I_{m1} + 5.65\angle45 I_{m2} = -60\angle-90 \end{cases}$$

$$I_{m1} = \frac{\begin{vmatrix} 20\angle-90 & -4\angle90 \\ -60\angle-90 & 5.65\angle45 \end{vmatrix}}{\begin{vmatrix} 2.5\angle36.89 & -4\angle90 \\ -7.21\angle33.7 & 5.65\angle45 \end{vmatrix}} = \frac{178.93\angle-153.47}{20.59\angle-29.08}$$

$$I_{m1} = 8.69\angle-124.4$$

$$V_1 = V_x = \underbrace{20\angle-90}_{V_s} - \underbrace{2\angle0}_{R} \underbrace{8.69\angle-124.4}_{I_{m1}} = 11.33\angle-29.95$$

$$V_1 \neq 11.33 \cos(2t - 29.95)$$

$$V_2 = V_1 - I_m, 2.5 \angle -90$$

$$V_2 = 11.33 \angle -29.95 - 8.69 \angle 124.4 \cdot 2.5 \angle -90 =$$

$$= 11.33 \angle -29.95 - 21.725 \angle -214.4 =$$

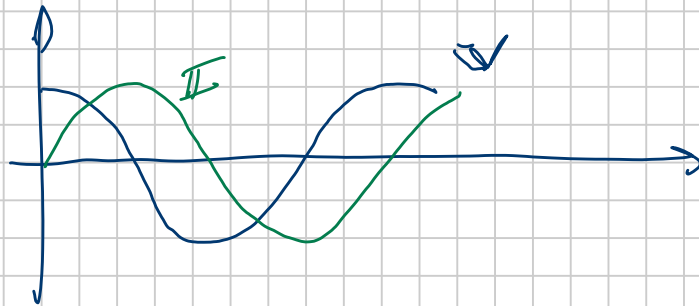
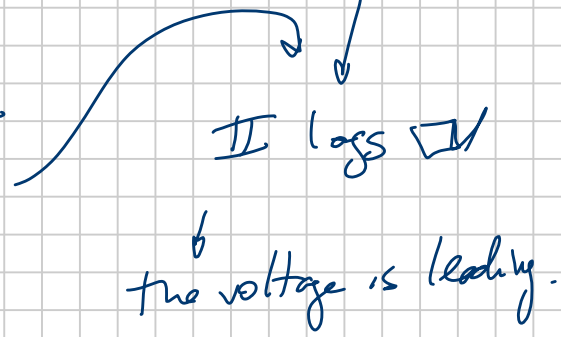
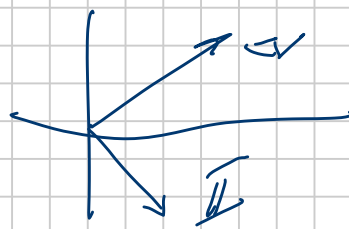
$$= 33.03 \angle -32.877$$

$$V_2(t) = 33.03 \cos(2t - 32.877)$$



Leading and lagging:

$\omega \rightarrow I = \frac{V}{\omega L} \angle 90^\circ = V(\omega L) \angle -90^\circ$



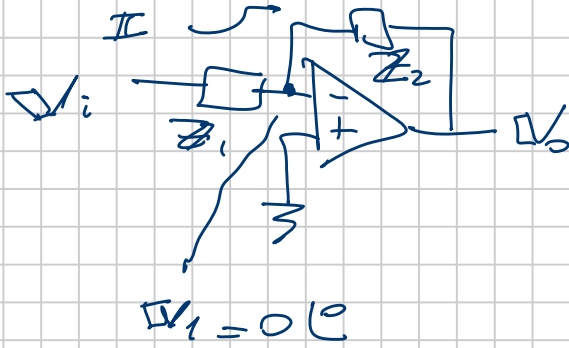
(with a capacitor the voltage is lagging)

with phasors, steady state analysis with sinusoids is like dc analysis

↳ Instead of R we use Z

So we can apply the same techniques: Norton equivalent
Thevenin "
superposition
source transformations
nodal analysis
mesh "

Operational amplifiers:



$$I = \frac{V_i}{Z_1} = -\frac{V_o}{Z_2}$$

$$\rightarrow \frac{V_o}{V_i} = -\frac{Z_2}{Z_1}$$

$$\text{If } \begin{cases} Z_2 = R_2 \\ Z_1 = R_1 \end{cases} \quad \left\{ \quad \frac{V_o}{V_i} = -\frac{R_2}{R_1} \quad \rightarrow \text{inverting amplifier} \right.$$

$$\text{If } \begin{cases} Z_2 = \frac{1}{\omega C} \angle -90^\circ \\ Z_1 = R \end{cases} \quad \left\{ \quad \frac{V_o}{V_i} = \frac{1}{\omega CR} \angle -90^\circ \right.$$

$$\text{If } V_i = V_i \angle \varphi_i$$

$$V_o = \frac{1}{\omega RC} \angle \varphi_i - 90^\circ$$

↳ Integrator

$$\int v(t) dt \quad \longleftrightarrow \quad \frac{V}{j\omega}$$

II

$$\begin{aligned} \varphi_2 &= R \\ \varphi_1 &= \frac{1}{\omega C} \quad (-90) \end{aligned}$$

$$\left\{ \frac{U_0}{U_i} = \omega CR \quad (90) \right.$$

↓
Differentiator