

Jonathan W. Valvano

October 8, 2010, 2:00pm-2:50pm.

(10) Question 1. Debugging dump.

Part a) This debugging monitor is *minimally intrusive*.

Part b) When defining intrusiveness, it is better to quantify exactly how much change the instrument affects the system being tested. This code only takes 20 cycles to execute. As a fraction, this is only 20/8000.

(bonus) For an inductor, $V = L \, dI/dt$ (FYI, the capacitor is $I = C \, dV/dt$)

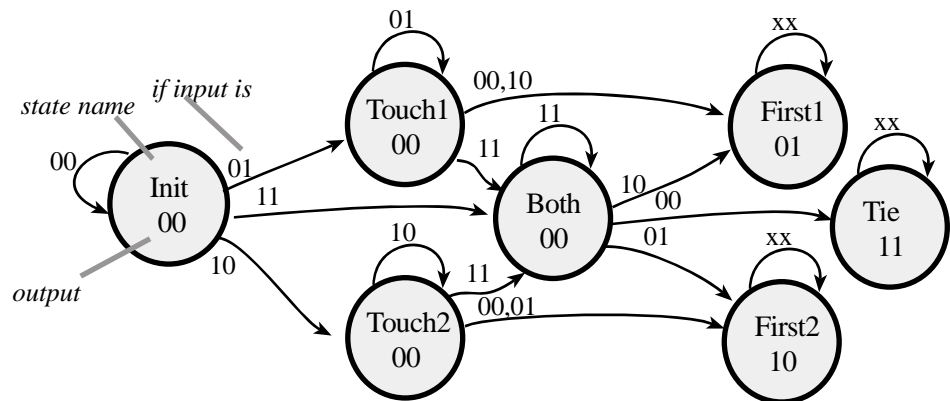
(15) Question 2. Critical sections may occur when there is a nonatomic read-modify-write access to a shared global. One cannot tell if software like `bReg = ~bOC1;` will be atomic without seeing the assembly code the compiler produces. The machine is not atomic with respect to lines of C, rather most assembly instructions are atomic.

```
short bOC1=0; // true if first ISR occurred first
short bReg=0; // true if first call to function occurred first
interrupt 9 void IC1handler(void){
    if((bReg==0)&&(bOC1==0)) bOC1 = 1; // interrupt first
    TFLG1 = 0x02; // acknowledge OC1
    Stuff1();
}
void RegularFunction(void){
asm sei // make atomic, to remove critical section
    if((bReg==0)&&(bOC1==0)) bReg = 1; // function first
asm cli
    Stuff2();
}
```

Solution that does NOT disable interrupts

```
short bOC1=0; // true if first ISR occurred first
short bReg=0; // true if first call to function occurred first
char bLooking=1; // true until first occurrence
interrupt 9 void IC1handler(void){
    if(bLooking){
        bLooking = 0; // stop looking
        bOC1 = 1; // interrupt was first
    }
    TFLG1 = 0x02; // acknowledge OC1
    Stuff1();
}
void RegularFunction(void){
asm clra //new value for bLooking
asm ldx #bLooking //pointer to bLooking
asm minm 0,x //in either case bLooking is now 0, carry set if used to be 1
asm bcc skip //skip if second program to execute
asm movw #1,bReg //regular function first
asm skip:
    Stuff2();
}
```

(20) Question 3. Draw a Moore FSM graph to solve the following problem.



(20) Question 4. The goal is to eliminate jitter. The proper solution occurs when one interrupt is time-shifted by $500 \mu\text{s}$ from the other interrupt.

Part a) Let t be an arbitrary time reference in ms. The OC1 interrupts occur (every 1 ms) at $t+1, t+2, t+3, \dots$. The OC2 interrupts occur (every 2 ms) at $t+1.5, t+3.5, t+5.5, \dots$

```
void Question5_Init(void){
    TSCR1 = 0x80;    // Enable TCNT 8 MHz in run mode
    TSCR2 = 0x03;    // divide by 8 TCNT prescale, 1us
    TIOS |= 0x06;    // activate TC1,TC2 as output compares
    TIE |= 0x06;     // arm OC1, OC2
    TC1 = TCNT+1000; // First OC1 in 1ms
    TC2 = TC1+500;   // First OC2 in 0.5ms after the OC1 interrupt
    TFLG1 = 0x06;    // clear both flags
    asm cli
}
```

Part b) If you acknowledge using `TFLG1 |= 0x02;` or `TFLG1 |= 0x04;` it will clear all 8 bits of `TFLG1`, which is very BAD. If you use code like `TC1 = TCNT+1000;`, then the interrupt period will not be accurate.

```
interrupt 9 void TC1handler(void){
    TFLG1 = 0x02;    // acknowledge OC1
    Task1();
    TC1 = TC1+1000; // execute Task 1 every 1ms
}
interrupt 10 void TC2handler(void){
    TFLG1 = 0x04;    // acknowledge OC2
    Task2();
    TC2 = TC2+2000; // execute Task 2 every 2ms
}
```

(10) Question 5. $n*1024$ must be less than 65535 to avoid overflow. Choose smallest error

`out = (12*in)/17;`

or `out = (12*in+8)/17;`

(15) Question 6. 100 mA will require the 2N2222 (because it can handle up to 500 mA of I_{CE}). We could have used any NPN with $I_{CE} > 100\text{mA}$, e.g., TIP120, IRF540. The V_{CE} on voltage of the 2N2222 is 0.3V. Because the current gain is 100 (h_{fe}) the base current needs to be $100\text{mA}/100 = 1\text{mA}$. The I_{OH} of the 9S12 can supply this 1mA (I_{OH} can be up to 10 mA). Because the V_{OH} of the 9S12 is 4.2V (or greater) and the V_{BE} if the 2N2222 is 0.6V (or less), the resistor from the 9S12 to the 2N2222 base must be less than $(4.2-0.6\text{V})/1\text{mA} = 3.6/0.001 = 3.6 \text{ k}\Omega$. I suggest making R much less than $3.6 \text{ k}\Omega$ (e.g., $2 \text{ k}\Omega$) because it will force the NPN into saturation, independent of the V_{OH} of the 9S12, the V_{BE} of the 2N2222, the h_{fe} of the 2N2222, and the resistance of the coil. Therefore, when the digital output is high, the voltage across the motor will be 5.7V. You might have been tempted to use a higher voltage supply, like the “Bad solution” and use a series resistor (R_2) to drop the voltage down to 5V. There are two fundamental problems with the “Bad solution”. First, the solution wastes power, the power delivered into R_2 is lost as heat. Second, the resistance of the coil is a function of the mechanical load on the electromagnet. The coil resistance can not be assumed to be constant.

